



**sureflow**<sup>®</sup>  
GATE VALVES  
FOR AUSTRALIAN WATERWORKS

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VIADUX VERSION 1.2

## GATE VALVES ON-OFF VALVES

### DESIGNED FOR THE PRIMARY FUNCTION OF FLOW ISOLATION

Gate valves feature a sliding partition that can be closed to block flow or opened fully for maximum flow.

Gate valves are used to isolate sections of pipelines, branch off-takes and pieces of equipment. They are on-off valves designed for the primary function of flow isolation and should only be operated in the fully closed or fully open positions. The sliding motion of the gate is effected by a rotating screw, known as a spindle or stem.

Sluice valves are gate valves and prior to the introduction of fusion bonded coatings they were of a heavier construction to endure buried service applications, whereas gate valves were associated with above ground applications. Today's modern coating systems remove the need for distinction between buried and above ground applications and therefore no need for sluice valve and gate valve distinction.



There is a growing industry trend to use gate valves in flow regulating and scour applications. When gate valves are used in these applications it is essential that they are operated in the fully opened position and any regulation of flow controlled by other means, such as orifice plates.

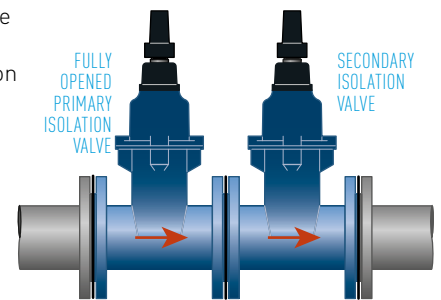
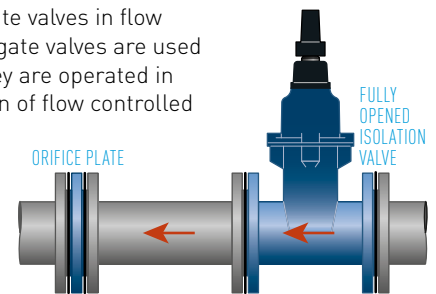
Orifice plates choke the flow and reduce head loss across the gate valve thus preventing valve damage.

Gate valves should not be used for throttling or adjusting flow as associated turbulence and high velocity can lead to vibration, chattering and fretting wear, as well as cavitation damage of the valve and downstream pipeline.

When used as a control or modulating valve this can also lead to these problems, the installation of a secondary valve for isolation purposes is recommended.

Secondary isolation valve used for control or modulating purposes. Primary isolation valve used for isolation purposes only.

When throttling is necessary, globe or butterfly valves should be used.

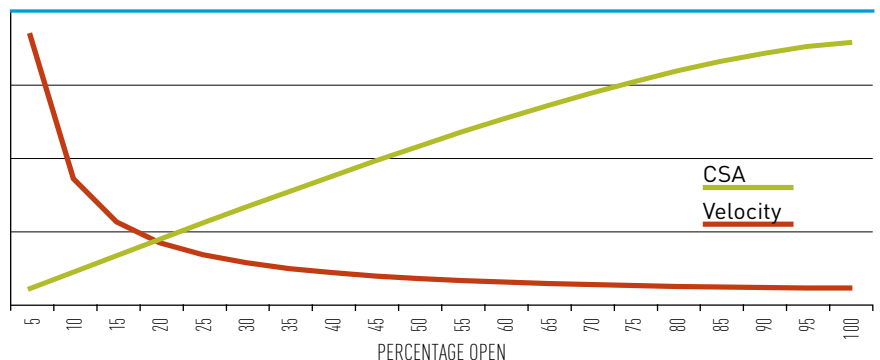


### THROTTLING

When gate valves are fully opened their head loss coefficient  $K_L$  is in order of 0.12.

Note. The flow through the valve is not directly proportional to the number of turns of the valve spindle.

### CSA - VELOCITY VS PERCENTAGE OPEN



# GATE VALVES DESIGN OPTIONS

## METAL SEATED OR RESILIENT SEATED

There are two design options for Gate Valves, Metal Seated and Resilient Seated. These two options can also be split into two categories Non-Rising Spindle (Inside Screw) and Rising Spindle (Outside Screw).

Non-Rising Spindle Gate valves are suitable for above ground and underground installations but are used predominately in underground installations because spindle movement is rotational only and additional cover is not required to accommodate the opened valve.

Rising Spindle Gate valves are predominately used for above ground and valve pit installations. They are commonly used in fire service applications where a positive indication of the open or closed position is necessary.

The SUREFLOW® range of Gate Valves employs an articulated gate design where the wedge nut is located separately within a housing in the gate. This articulated gate design has key advantages over systems where the stem nut is integral with the gate. It overcomes the risk of damage through direct pressure on the stem, stem nut or other components during operation or transitional throttling.



The use of gate valves for end of line isolation is not recommended. If the valves are to be fitted to the end of a line we recommend the use of a blank flange or plug to ensure isolation of the line.

### METAL SEATED GATE VALVES

Metal seated gate valves comprise a metal gate, typically wedge shaped and made of gunmetal for valves up to and including 200mm and ductile iron with gunmetal sealing rings for larger sizes.

The gate and body are fitted with metal sealing rings by threading or plastic deformation to prevent loosening in service. A continuous seal is provided behind the rings to prevent corrosion.

The valve is closed by appropriate rotation of the spindle which drives the gate down between the sealing rings. Sealing is effected by the mating of the sealing rings. Sometimes the sealing surfaces can become damaged from the impact of foreign debris or from foreign debris being lodged between the sealing faces.

Throttling of a metal seated gate valve is the most common cause of damage to the sealing faces. Repair of the sealing surfaces is not a simple operation and a factory refit is normally necessary.

In metal seated gate valves, maximum torque on the spindle is associated with initial opening or 'cracking' of the valve. Properly operated and closed, these valves can effect a drop tight seal but leakage rates of 2-10 ml/min are acceptable under AS 2638.1.

### RESILIENT SEATED GATE VALVES

Resilient seated gate valves contain an EPDM rubber encapsulated ductile iron gate. The valve is closed by appropriate rotation of the spindle which drives the gate against the cast internal sealing surfaces of the valve body. These surfaces are normally coated with fusion bonded polymers such as epoxy or nylon.

Sealing is achieved by the compression of the EPDM rubber coating on the gate against the valve body. In resilient seated gate valves, maximum torque of the spindle is associated with closing the valve to overcome the effects of friction and compression of the EPDM rubber coating.

Properly operated and closed, these valves can effect a drop tight seal.

The gate is body guided throughout its closure and secondary guides become effective near the end of its travel to ensure correct seat alignment.



## GATE VALVES BELOW GROUND

### FIGURE 500 RESILIENT SEATED

Ductile iron body and bonnet for high strength and impact resistance

Ductile iron gate fully encapsulated in EPDM rubber to ensure drop tight sealing

Grade 431 Stainless Steel spindle for high strength and corrosion resistance

Gunmetal dezincification resistant top casting incorporating dual O-ring seals and wiper ring for long life operation

Back seal facility to allow for replacement of seals under full operating pressure

Fusion Bonded Polymeric coating for long life corrosion protection

Straight through full bore to avoid debris traps

Isolated fasteners for corrosion protection

Anti-friction thrust washer for low operating torques

Integral cast in feet for safe and easy storage

Integral lifting lugs for installation convenience

Anticlockwise closing or clockwise closing available

Key, handwheel or gearbox operation available



### AUSLITE RESILIENT SEATED

Ductile Iron body and bonnet for high strength and impact resistance

Ductile Iron gate fully encapsulated in EPDM elastomer to ensure drop tight sealing

Grade 431 stainless steel spindle for high strength and corrosion resistance

Seal housing incorporates dual o-ring seals and wiper ring for long life operation

Back seal facility to allow for replacement of seals under full operating pressure

Fusion bonded polymeric coating for long life corrosion protection

Straight through full bore to avoid debris traps

Isolated fasteners for corrosion protection

Anti-friction guide liners for low operating torques

Integral cast-in feet for safe and easy storage

Anticlockwise closing or clockwise closing available

Key or handwheel operation



### FIGURE 400 METAL SEATED

Ductile Iron body and bonnet for high strength and impact resistance

Solid gunmetal gate for DN 80 - DN 200, ductile iron fusion coated gate with gunmetal rings for larger sizes TWS400/1/07

Grade 431 stainless steel spindle for high strength and corrosion resistance

Gunmetal dezincification resistant top casting incorporating dual o-ring seals and wiper ring for long life operation

Back seal facility to allow for replacement of seals under full operating pressure

Fusion Bonded Polymeric coating for long life corrosion protection

Isolated fasteners for corrosion protection

Anti-friction thrust washer for low operating torques

Integral cast in feet for safe and easy storage

Integral lifting lugs for installation convenience

Anticlockwise closing or clockwise closing available

Key, handwheel or gearbox operation available



# GATE VALVES ABOVE GROUND

## FIGURE 500H + 500R RESILIENT SEATED

Ductile Iron body and bonnet for high strength and impact resistance

Ductile iron gate fully encapsulated in EPDM rubber to ensure drop tight sealing

Grade 431 stainless steel spindle for high strength and corrosion resistance

Gunmetal dezincification resistant top casting incorporating dual O-ring seals and wiper ring for long life operation

Back seal facility with 500H configuration to allow for replacement of seals under full operating pressure

Fusion Bonded Polymeric coating for long life corrosion protection

Straight through full bore to avoid debris traps

Isolated fasteners for corrosion protection

Anti-friction thrust washer for low operating torques

Integral cast in feet for safe and easy storage

Integral lifting lugs for installation convenience

Handwheel operation



## FIGURE 600H + 601 METAL SEATED

Ductile Iron body and bonnet for high strength and impact resistance

Solid gunmetal gate for DN 80 – DN 200, ductile iron fusion coated wedge with gunmetal rings for larger sizes

Grade 431 stainless steel spindle for high strength and corrosion resistance

Gunmetal dezincification resistant top casting incorporating dual O-ring seals and wiper ring for long life operation

Back seal facility with 600H configuration to allow for replacement of seals under full operating pressure

Fusion Bonded Polymeric coating for long life corrosion protection

Isolated fasteners for corrosion protection

Anti-friction thrust washer for low operating torques

Integral cast in feet for safe and easy storage

Integral lifting lugs for installation convenience

Hand wheel operation



## GATE VALVES TECHNICAL DATA

		BELOW GROUND			ABOVE GROUND	
		Fig 400	Fig 500	AUSLITE	Fig 500H Fig 500R	Fig 600 Fig 601
Class	PN	16 or 35	16	16 or 25	16	16
Size range	DN	80 - 1000	80 - 600	80 - 300	80 - 300	80 - 300
Allowable operating temperature (AOP)	°C	40	40	40	40	40
End connections						
Flanged - AS 2129 TE		✓	✓	✓ <sup>2</sup>	✓	✓
- AS 4087 Fig B5		✓	✓	✓	✓	✓
- AS 4087 Fig B6		✓	✓ <sup>1</sup>	✓ <sup>2</sup>		
Note: ISO, ANSI and other drillings available on request.						
TYTON JOINT						
- Socket		✓ <sup>3</sup>	✓ <sup>6</sup>	✓ <sup>9</sup>		
- Spigot - AS/NZS 2280		✓ <sup>4</sup>	✓ <sup>7</sup>	✓		
Shouldered		✓ <sup>5</sup>		✓ <sup>10</sup>		
Flange/Socket			✓ <sup>8</sup>	✓		

### APPROVALS

WSAA Appraisal No. 10/17	✓ <sup>11</sup>	✓	✓	✓	✓
ISC AS 2638 Product Mark Reg. No. PRD/R61/0412/2	✓ <sup>11</sup>	✓	✓	✓	✓
Certified to AS 4020 - suitable for contact with drinking water	✓	✓	✓	✓	✓

### CERTIFICATIONS

ISC AS 2638 Certified Product  
Licence No. PRD/R61/0412/2



WaterMark Level 1  
AS 2638.1/AS 2638.2  
ISC-WM-030028-101-R00

### NOTES

- PN 25 Fig 500 Valves are available in DN 100 and DN 150 sizes in flanged versions only
- AS 2129 TE and PN 25 Auslrite Valves are available in DN 80, DN 100 and DN 150 flanged versions only
- Fig 400 Socket Valve available in DN 100 - DN 250 sizes only
- Fig 400 Spigot Valves available in DN 100 and DN 150 sizes only
- Fig 400 Shouldered Valves available in DN 100 and DN 150 sizes only
- Fig 500 Socket Valves available in DN 100 - DN 375 sizes only
- Fig 500 Spigot Valves available in DN 80 - DN 300 sizes only
- Fig 500 Flange/Socket Valves available in DN 80 - DN 300 sizes only
- AUSLITE Socket Valves available in DN 100 and DN 150 sizes only
- AUSLITE Shouldered Valves available in DN 100 and DN 150 sizes only
- Approvals for DN 80 - DN 750 sizes only



# GATE VALVES GEARBOXES

Gate valves are normally supplied without gearing. Gearboxes are fitted when the operator applied spindle torque (turning moment) is greater than that which can be reasonably achieved manually by field staff. These torque thresholds may be set by operator, OH&S or legislative requirements.

The need for a gearbox is determined by:

- operating pressure
- valve diameter
- differential pressure across the gate
- valve orientation in service – horizontal or vertical
- maximum operator input torque
- maximum possible input torque to the valve

Where gearboxes are required, sizes DN 250 to DN 600 valves are supplied with single input shaft. For DN 750 to DN 1000 valves, dual input shafts with a dial indicator are fitted. Dial indicators are not suitable for open weather installations.

Please contact your local Viadux Customer Centre for advice.

## TORQUE REQUIREMENTS OF METAL SEATED GATE VALVES

The figure below shows how torque (spindle turning force) varies as a MSGV is opened and closed.

If there is a differential head across the gate in the closed position the initial opening torque, also known as the 'cracking' torque, is very high. This is due to the additional friction component generated between the body sealing rings and gate sealing rings by the unbalanced pressure.

As the valve is opened, the torque falls rapidly as the differential head across the valve drops off. The 'opening' torque corresponds to the spindle turning force required to overcome continued opening and final friction of the gate sealing rings. The torque continues to fall to a constant value known as the 'running' torque or 'functional' torque where the operational torque is at a minimum.

'Closing' torque is much less than the 'cracking' torque. When closing a metal seated gate valve it should be remembered that sealing is effected by unbalanced pressure against the wedge rings bearing against the body rings. Backing off of the stem by ½ turn after full closure may be necessary to settle the rings into a fully seated and mated position.

## GEARBOX SIZING FOR METAL SEATED GATE VALVES

Gearbox sizing based on the cracking torque is not recommended as the resulting high ratio gearboxes make operating times very long. Gearboxes should preferably be sized on the running torque as the 'cracking' torque is only required for initial opening of the valve and lasts for ¼ to 1 turn of the spindle.

It should be noted however that torques in excess of the minimum strength test torque may damage the valve. Where high ratio gearboxes are necessary, torque limiting devices should be considered.

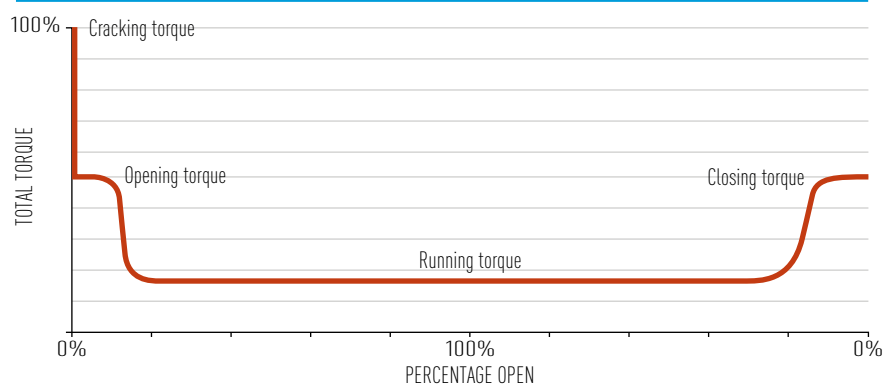
Determining 'running' torque is difficult and use of 'maximum functional test torque' to size the gearbox is common. Sizing the gearbox on running or functional torque may require torque in excess of the nominated maximum operator input torque to crack the valve. Cracking torque may be overcome with a longer bar, torque multiplier or more operators.

Standard gearbox ratios include 2:1, 4:1, 6:1, 12:1, 16:1 and 24:1.

High ratio gearboxes require low operating torques but require extra turns to operate the valve and increase risk of valve damage due to excessive input torque.

Low ratio gearboxes reduce the risk of damage and require less turns to operate the valve but require high input torques, particularly for cracking.

## TYPICAL MSG VALVE TORQUE VARIATION



# GATE VALVES GEARBOXES

## MINIMUM REQUIRED GEARBOX RATIO FOR METAL SEATED GATE VALVES. G

- $G = T_f / (T_m E)$
- G = minimum required gearbox ratio, rounded up to 2, 4, 6, 12, 16, 24
- $T_f$  = maximum functional test torque or running torque
- E = gearbox efficiency, single reduction spur = 0.90; single reduction bevel = 0.85
- $T_m$  = maximum operator input torque

### EXAMPLE

DN 450 PN16 metal seated gate valve coupled with spur gearbox

- $T_f = 425\text{Nm}$  (maximum functional test torque - AS2638.1)
- E = 0.90
- $T_m = 150\text{Nm}$  (assumed maximum operator input torque)
- $G = 425 / (150 \times 0.90)$   
= 3.14
- Maximum required gearbox ratio,  
G = 4 (rounded up)

## MAXIMUM ALLOWABLE GEARBOX INPUT TORQUE FOR METAL SEATED GATE VALVES

- $T_{mg} = T_{ms} / (GE)$
- $T_{mg}$  = maximum allowable gearbox input torque
- G = selected gearbox ratio
- E = gearbox efficiency
- $T_{ms}$  = minimum strength torque test

### EXAMPLE

DN 450 PN16 metal seated gate valve coupled with spur gearbox

- $T_{ms} = 1275\text{Nm}$  (minimum strength torque test - AS2638.1)
- E = 0.90
- G = 4 (from above example)
- $T_{mg} = 1275 / (4 \times 0.9)$   
= 354Nm
- Maximum allowable gearbox input torque  
= 354Nm

## FINAL CHECK FOR METAL SEATED GATE VALVES

Check to ensure that cracking the valve is possible with torques less than  $T_{mg}$  with the selected gearbox ratio.

If  $T_{mg}$  is practicable, it can be assumed the valve can be cracked with the chosen gearbox even though an applied input torque is larger than the specified maximum operator input torque. This is because cracking torque is always less than minimum strength test torque.

If  $T_{mg}$  is greater than a practicable input torque, the gearbox output torque should be calculated, based on the maximum possible input torque.

- $T_{go} = T_p G E$
- $T_{go}$  = gearbox output torque
- $T_p$  = maximum possible input torque
- G = gearbox ratio
- E = gearbox efficiency

$T_{go}$  should be greater than the nominated cracking torque. If not, a higher ratio gearbox should be selected and  $T_{mg}$  recalculated. Repeat the process until  $T_{mg}$  is accepted as a practicable input torque OR until  $T_{go}$  is greater than the nominated cracking torque.

### EXAMPLE

DN 450 PN16 metal seated gate valve coupled with spur gearbox. (Calculated cracking torque for a DN 450 PN16 metal seated gate valve at 1600kPa is 520Nm)

- $T_p = 250\text{Nm}$  (assumed maximum possible input torque)
- E = 0.90
- G = 4 (from above example)
- $T_{go} = 250 \times 4 \times 0.9$   
= 900Nm
- Gearbox output torque  
= 900Nm  
which is greater than the calculated cracking torque of 520Nm. Therefore gearbox selection is acceptable.

## TORQUE REQUIREMENTS OF RESILIENT SEATED GATE VALVES

The figure on page 9 shows how torque (spindle turning force) varies as a RSGV is opened and closed. The torque to seal a resilient seated valve is significantly higher than the torque to open.

During opening the torque to operate reduces as the differential head across the gate reduces. The opening torque is also assisted by decompression of the EPDM rubber encapsulating the gate. Finally a steady state is reached at a minimum, known as the running torque.

Maximum torque for resilient seated gate valves is experienced on closing as the EPDM rubber coated wedge is compressed against the sealing interface in the valve body. The torque required to effect a full seal increases as friction and the compression increases at the end of travel of the gate.

## GEARBOX SIZING FOR RESILIENT SEATED GATE VALVES

Gearbox sizing based on torque to seal is not recommended as the resulting high ratio gearboxes make operating times very long. Gearboxes should preferably be sized on running torque as torque to seal is only required during closing of the valve and lasts for ¼ to 1 turn of the spindle.

It should be noted however that torques in excess of the minimum strength test torque may damage the valve.

Where high ratio gearboxes are necessary, torque limiting devices should be considered.

Determining 'running' torque is difficult and use of 'maximum functional test torque' to size the gearbox is common. Sizing the gearbox on running or functional torque may require torque in excess of the nominated maximum operator input torque to seal the valve. Sealing torque may be overcome with a longer bar, torque multiplier or more operators.

Standard gearbox ratios include 2:1, 4:1 and 6:1.



# GATE VALVES GEARBOXES

## MAXIMUM ALLOWABLE GEARBOX INPUT TORQUE FOR RESILIENT SEATED GATE VALVES

## FINAL CHECK FOR RESILIENT SEATED GATE VALVES

High ratio gearboxes require low operating torques but require extra turns to operate the valve and increase risk of valve damage due to excessive input torque.

Low ratio gearboxes reduce the risk of damage and require less turns to operate the valve but require high input torques, particularly for sealing.

### MINIMUM REQUIRED GEARBOX RATIO FOR RESILIENT SEATED GATE VALVES. G

$$G = T_f / (T_m E)$$

G = minimum required gearbox ratio, rounded up to 2, 4, 6

T<sub>f</sub> = maximum functional test torque or running torque

E = gearbox efficiency, single reduction spur = 0.90; single reduction bevel = 0.85

T<sub>m</sub> = maximum operator input torque

#### EXAMPLE

DN 450 PN16 resilient seated gate valve coupled with spur gearbox

$$T_f = 540\text{Nm (running torque)}$$

$$E = 0.90$$

$$T_m = 150\text{Nm (assumed maximum operator input torque)}$$

$$G = 540 / (150 \times 0.90) = 4$$

Maximum required gearbox ratio,

$$G = 4$$

$$T_{mg} = T_{ms} / (GE)$$

T<sub>mg</sub> = maximum allowable gearbox input torque

G = selected gearbox ratio

E = gearbox efficiency

T<sub>ms</sub> = minimum strength torque test

#### EXAMPLE

DN 450 PN16 resilient seated gate valve coupled with spur gearbox

$$T_{ms} = 1800\text{Nm (minimum strength torque test - AS 2638.2)}$$

$$E = 0.90$$

$$G = 4 \text{ (from above example)}$$

$$T_{mg} = 1800 / (4 \times 0.9) = 500\text{Nm}$$

Maximum allowable gearbox input torque = 500Nm

Check to ensure that the torque to seal the valve is possible with torques less than T<sub>mg</sub> with the selected gearbox ratio. If T<sub>mg</sub> is practicable, it can be assumed the valve can be sealed with the chosen gearbox even though an applied input torque is larger than the specified maximum operator input torque. This is because torque to seal is always less than minimum strength test torque.

If T<sub>mg</sub> is greater than a practicable input torque, the gearbox output torque should be calculated, based on the maximum possible input torque.

$$T_{go} = T_p G E$$

T<sub>go</sub> = gearbox output torque

T<sub>p</sub> = maximum possible input torque

G = gearbox ratio

E = gearbox efficiency

T<sub>go</sub> should be greater than the nominated torque to seal. If not, a higher ratio gearbox should be selected and T<sub>mg</sub> recalculated.

Repeat the process until T<sub>mg</sub> is accepted as a practicable input torque OR until T<sub>go</sub> is greater than the nominated sealing torque.

#### EXAMPLE

DN 450 PN16 resilient seated gate valve coupled with spur gearbox (assume nominated torque to seal is equal to the maximum functional test torque)

$$T_p = 250\text{Nm (assumed maximum possible input torque)}$$

$$E = 0.90$$

$$G = 4 \text{ (from above example)}$$

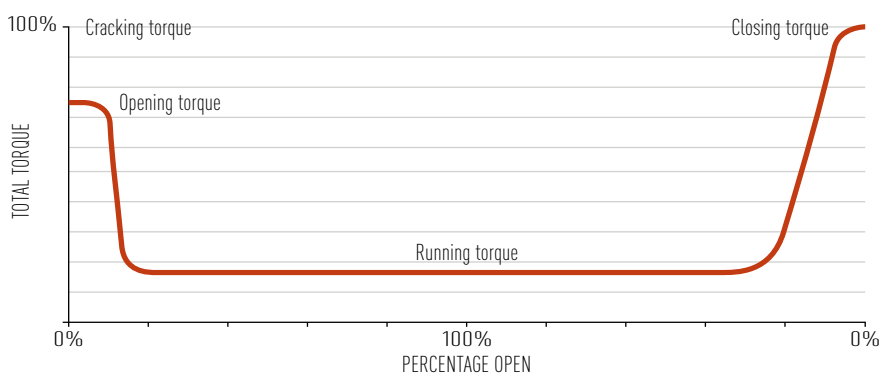
$$T_{go} = 50 \times 4 \times 0.9 = 900\text{Nm}$$

Gearbox output torque

$$= 900\text{Nm}$$

which is greater than the maximum functional test torque of 600Nm. Therefore gearbox selection is acceptable.

### TYPICAL RSG VALVE TORQUE VARIATION



## GATE VALVES IDENTIFICATION OF CLOSING DIRECTION



**BLACK CAP**

Indicates anti-clockwise closing.



**RED CAP**

Indicates clockwise closing



**HANDWHEEL**

An arrow on the top of a handwheel also indicates the closing direction.

## VALVE END CONNECTIONS



**FLANGE - FLANGE**

DN 80  
- DN 1000



**FLANGE - SOCKET**

DN80 - DN300



**SOCKET - SOCKET**

DN100  
- DN375



**SPIGOT - SPIGOT**

DN80  
- DN300



**SHOULDERED END**

DN100,  
DN150

# GATE VALVES TROUBLESHOOTING

## LEAKAGE

Check and confirm that the appropriate torque has been applied to the valve spindle. Service the following areas as applicable:

### SPINDLE

The spindle seals are elastomeric O-rings. They can be replaced while the valve remains in-line under pressure by opening the gate fully.

### SEAT-MSGV

Foreign matter may be trapped between the wedge and body sealing rings. A leak in the 6 o'clock position suggests the gate has not been fully homed. Close the valve fully to the recommended closing torque. If the leak persists, open the valve just a little to allow a high velocity flow to flush the debris from the seat. This process may have to be repeated several times. A leak in the 12 o'clock position suggests the gate has been overtightened. It may be necessary to back the stem off by a ½ turn to allow the rings to settle into the fully seated and mated position. Failing this, open the valve and check for damage to the body and gate sealing rings. If damaged, return the valve to Viadux for repair.

### SEAT-RSGV

As for MSGV except for gate inspection, check EPDM rubber encapsulated wedge. If it is damaged or severely cut, replace the wedge.

### BOLTED CONNECTIONS

Inspect for loose bonnet-to-body screws or spindle seal retainer screws and tighten as necessary with gate in open position. If the line is pressurized, pressure should be relieved prior to tightening any screws. Reinstall all screws and tighten alternately to the recommended torque. Do not tighten screws past their yield strength. After successfully passing hydro test, reinstate fastener sealant.

## LEAKAGE DURING TESTING

Resilient seated gate valves per AS 2638.2 have a zero allowable leakage rate.

Metal seated gate valves have an allowable leakage defined in AS 2638.1 Table 5.2.

If seat leakage is detected, it may be due to trapped air or foreign material in the line. Open the valve enough to get high velocity flow to flush out valve. Repeat several times until leakage stops.

If testing between valves, allow enough time to fill the pipeline and vent off air.

If pressure testing requirements exceeds AOP of valve, testing should be carried out with the gate in open position to prevent damage to the valve.

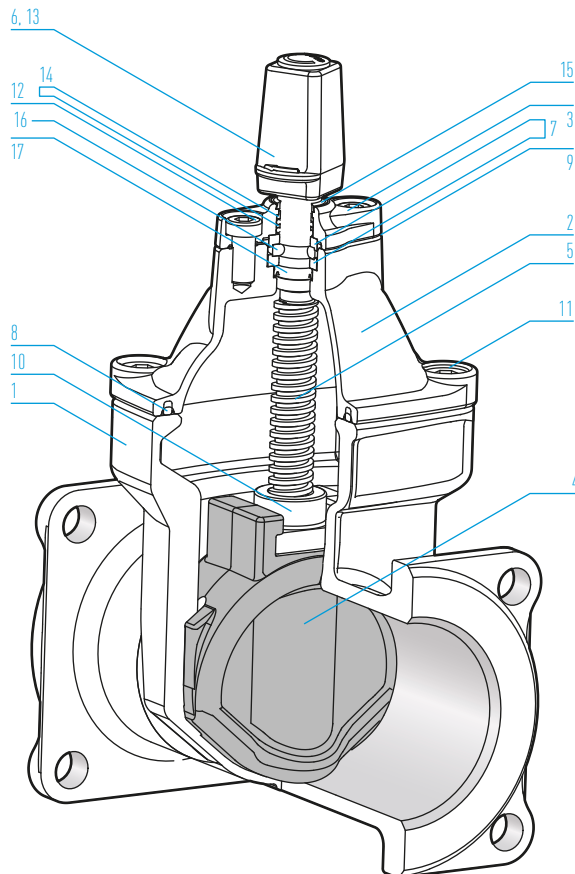
Class of valve	PN	16	25	35
Allowable Operating Pressure	kPa	1600	2500	3500

## VALVE SERVICE EFFECTS

Over-torquing can permanently damage the operating parts of a valve. Over-torquing commonly results from misuse of portable actuators. These machines should be adjusted to ensure the output torque is suitable for the valve size. The cracking/opening turns should be done manually and the actuator applied for the running torque only.

If valve has not been operated periodically, excessive buildup could occur that would affect valve operation. The valve should be exercised one turn at a time and cycled from open to closed as necessary to attempt removal of internal buildup.

## AUSLITE® GATE VALVES RESILIENT SEATED PARTS LIST

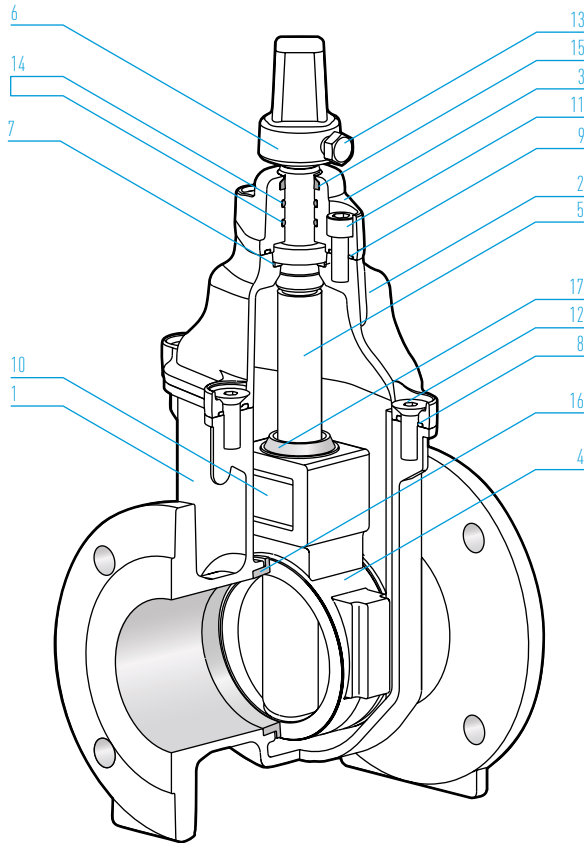


No	Description Material / Standard
1	Body Ductile Iron / Fusion Bonded Polymeric Coating AS 1831 400-15 min / AS 4158
2	Bonnet Ductile Iron / Fusion Bonded Polymeric Coating AS 1831 400-15 / AS 4158
3	Retaining Plate Stainless Steel / ASTM A276 316 / 431
4	Wedge Ductile Iron (EPDM Encapsulated) / AS 1831 400-15 min
5	Stem Stainless Steel / ASTM A276 431
6	Stem Cap Ductile Iron / AS 1831 400-15 min
7	Backseal / Collar Retainers Copper Alloy – Dezincification Resistant / AS 1567 C48600 min / C69300 min
8	Body Gasket EPDM / AS 1646
9	Top Gasket EPDM / AS 1646
10	Wedge Nut Copper Alloy – Dezincification Resistant / AS 1567 C48600 min
11	Counter Sunk Screw and Isolation Stainless Steel / ASTM A276 316 / Silicon
12	Socket Head Cap Screw and Isolation Stainless Steel / ASTM A276 316 / Silicon
13	Stem Cap Retaining Screw Stainless Steel / ASTM A276 316
14	O-Ring Nitrile Rubber / AS 1646
15	Wiper Ring EPDM / AS 1646
16	Collar Set / Copper Alloy – Dezincification Resistant / AS 1567 C69300 min
17	Backseal Ring Nitrile Rubber / AS 1646 min



# SUREFLOW® GATE VALVES

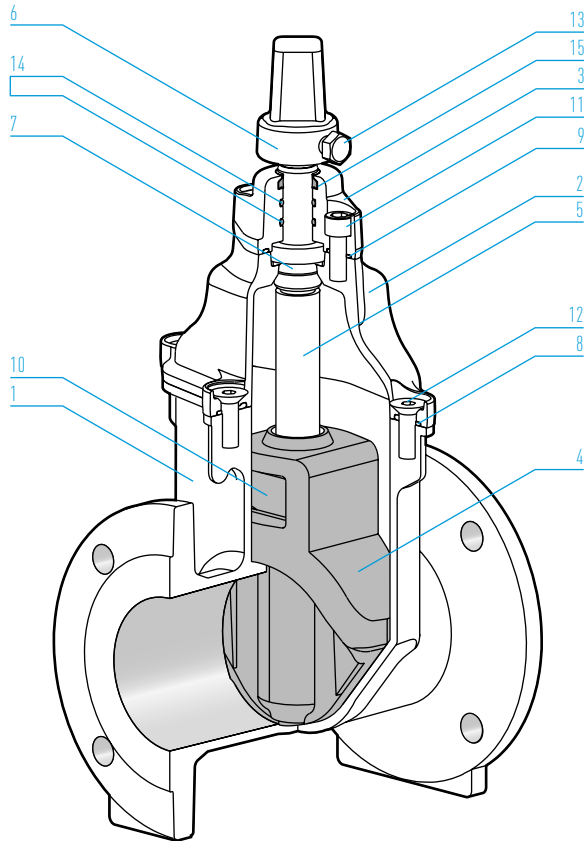
## METAL SEATED PARTS LIST



No	Description Material / Standard
1	Body Ductile Iron / Fusion Bonded Polymeric Coating AS 1831 400-15 min / AS 4158
2	Bonnet Ductile Iron / Fusion Bonded Polymeric Coating AS 1831 400-15 / AS 4158
3	Seal Retainer Gunmetal / AS 1565 C83600
4	Gate DN 80 – DN 200 Gunmetal / AS 1565 C83600 DN 225 – DN 1000 Ductile Iron / AS 1831 400-15 min
5	Spindle Stainless Steel / ASTM A276 431
6	Spindle Cap Ductile Iron / AS 1831 400-15
7	Thrust Washer Acetal
8	Body Gasket EPDM / AS 1646
9	Bonnet Gasket EPDM / AS 1646
10	Gate Nut Gunmetal / AS 1565 C83600
11	Socket Head Cap Screw and Isolation Stainless Steel / ASTM A276 316
12	Counter Sunk Screw and Isolation Stainless Steel / ASTM A276 316
13	Hex Head Screw Stainless Steel / ASTM A276 316
14	O-Rings Nitrile Rubber / AS 1646
15	Wiper Ring Nitrile Rubber / AS 1646
16	Seat Rings Gunmetal / AS 1565 C83600
17	Backseal Grommet Nitrile Rubber / AS 1646

# SUREFLOW® GATE VALVES

## RESILIENT SEATED PARTS LIST



No	Description Material / Standard
1	Body Ductile Iron / Fusion Bonded Polymeric Coating AS 1831 400-15 min / AS 4158
2	Bonnet Ductile Iron / Fusion Bonded Polymeric Coating AS 1831 400-15 / AS 4158
3	Seal Retainer Gunmetal / AS 1565 C83600
4	Gate Ductile Iron (EPDM Encapsulated) AS 1831 400-15
5	Spindle Stainless Steel / ASTM A276 431
6	Spindle Cap Ductile Iron / AS 1831 400-15
7	Thrust Washer Acetal
8	Body Gasket EPDM / AS 1646
9	Bonnet Gasket EPDM / AS 1646
10	Gate Nut Gunmetal / AS 1565 C83600
11	Socket Head Cap Screw and Isolation Stainless Steel / ASTM A276 316
12	Countersunk Screw and Isolation Stainless Steel / ASTM A276 316
13	Hex Head Screw Stainless Steel / ASTM A276 316
14	O-Rings Nitrile Rubber / AS 1646
15	Wiper Ring Nitrile Rubber / AS 1646

# GATE VALVES

## GLOSSARY

### ALLOWABLE OPERATING PRESSURE (AOP)

The allowable internal pressure, excluding surge, that a component can safely withstand in service

### ALLOWABLE SITE TEST PRESSURE (ASTP)

The maximum internal hydrostatic pressure that can be applied on site to a component in a newly installed pipeline

### MAXIMUM ALLOWABLE GEARBOX INPUT TORQUE

The maximum allowable input torque, which can be applied to a gearbox so that the output torque does not exceed the minimum strength test torque

### MAXIMUM ALLOWABLE OPERATING PRESSURE (MAOP)

The maximum internal pressure, including surge that a component can safely withstand in service

### MAXIMUM FUNCTIONAL TEST TORQUE

The maximum allowable torque to operate an ungeared gate valve at fully unbalanced allowable operating pressure

### MAXIMUM OPERATOR INPUT TORQUE

The purchaser-specified maximum operator input torque required to operate the valve or gearbox

### MAXIMUM POSSIBLE INPUT TORQUE

The maximum torque that can be practically applied by an operator either manually or by mechanical means

### MINIMUM STRENGTH TEST TORQUE

The minimum input torque an ungeared gate valve is designed to withstand

### NON-RISING SPINDLE DESIGN

A valve design where the gate is fixed to the spindle with a threaded nut, such that as the gate moves from closed to open position the spindle does not rise during operation

### PRESSURE CLASSIFICATION (PN)

A classification of valves by a PN number based on the allowable operating pressure expressed in hundreds of kilopascals

### RISING SPINDLE DESIGN

A valve design where the gate is fixed to the spindle such that as the gate moves from closed to open position the spindle rises during operation

## ALLOWABLE PRESSURES

PN		16	25	35
AOP	kPa	1600	2500	3500
MAOP1	kPa	1920	3000	4200
ASTP2	kPa	2000	3125	4375

### NOTES

- 1 Seat leakage may occur at maximum allowable operating pressures: however, structural damage should not occur
- 2 ASTP shall only be applied with the gate in the fully opened position



# sureflow<sup>®</sup>

## GATE VALVES

### PROJECT OFFICE

#### SYDNEY

P: 02 9794 3440  
F: 02 9794 3499  
E: projects@viadux.com.au

### CUSTOMER CENTRES

#### TOWNSVILLE

P: 07 4725 5940  
F: 07 4725 4995  
E: cct.sales@viadux.com.au

#### SOUTH EAST QUEENSLAND

P: 07 5589 4400  
F: 07 5534 7079  
E: ccseq.sales@viadux.com.au

#### NEWCASTLE

P: 02 4914 0700  
F: 02 4966 8776  
E: ccn.sales@viadux.com.au

#### SYDNEY

P: 02 9794 3440  
F: 02 9794 3499  
E: ccs.sales@viadux.com.au

#### MELBOURNE

P: 03 9309 9133  
F: 03 9309 6237  
E: ccm.sales@viadux.com.au

#### ADELAIDE

P: 08 8340 3411  
F: 08 8340 3422  
E: cca.sales@viadux.com.au

#### PERTH

P: 08 9346 8500  
F: 08 9346 8501  
E: ccp.sales@viadux.com.au

#### DARWIN

P: 08 8935 3300  
F: 08 8947 3981  
E: ccd.sales@viadux.com.au

**VIADUX PTY LTD** PO BOX 141 FAIRFIELD, NEW SOUTH WALES 1860 AUSTRALIA / VIADUX.COM.AU / PHONE 1300VIADUX

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